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# Investigation of the hyperfine structure of Ta I lines (VI)

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**Abstract.** We have classified about 200 new lines and have discovered 13 energy levels with even parity and 1 level with odd parity by means of the systematic hyperfine structure investigation of a large number of spectral lines of the neutral tantalum atom. For the new levels we deduced their angular momenta, parity and magnetic hyperfine interaction constants A as well as the electric quadrupole interaction constants B.

PACS. 32.10.Fn Fine and hyperfine structure

# 1 Introduction

During several years the hyperfine structure (hfs) of tantalum spectral lines have been investigated. In spite of all those efforts and their results the analysis of the tantalum spectrum is far from being complete. In a successful cooperation, we and groups from Hamburg and Poznan (Poland) [1–3] continued to analyse Ta spectra and to classify lines. Many of the lines investigated in this work are up to now unknown Ta lines, discovered on spectral plates which were exposed to the light of an Ar-Ta hollow cathode lamp using an Ebert monochromator (2 m focal length in fifth order). These spectra are taken by Arcimowicz [4]. Besides all those Ta lines listed in commonly used spectral tables [5-7], we found a large number of additional lines. Some of these lines coincide either with Ce or Tb lines listed in [5]. In order to check if our hollow cathode material contains traces of such elements, we looked for strong lines of Ce or Tb in our spectrum, but without success. Later on we could identify most of these lines as Ta lines. So we have to assume that some errors occurred in the designation of Ce and Tb lines in [5].

In the spectral range 4171–4485 Å we excited systematically one transition after the other by laser light; additionally some other lines have been investigated (see Tab. 1). If an excitation could be carried out, we received a characteristic hyperfine pattern, from which we could determine the hyperfine constants of lower and upper level of the transition. These constants were used as a "finger print" for the levels, which allowed us to identify without doubt the involved atomic levels. In some cases the investigations did lead to the discovery of previously unknown fine structure levels.

### 2 Experiment

The experimental arrangement was the same as used for our previous investigations [3]. Free tantalum atoms were produced by cathode sputtering in a tantalum hollow cathode lamp by the argon ions of the gas discharge. This source contains Ta atoms not only in the ground state, but also in higher excited states. With chopped radiation of a tunable cw dye laser free atoms could be excited. The laser-induced fluorescence (LIF) light was dispersed by a grating monochromator and detected with a photomultiplier using a lock-in amplifier. Sometimes the optogalvanic signal was also detected. For the accurate determination of the fluorescence wavelengths the fluorescence light was chopped with much higher frequency in front of the entrance slit of the monochromator and the discharge spectrum was recorded by means of a second lock-in amplifier simultaneously with the LIF signal.

# 3 Results and discussion

All wavelengths mentioned in this paper are given in unit Å in air. All energy levels were corrected with respect to their energetic position due to results of Engleman [8] obtained from Fourier transform spectra. With these corrections the wavelengths evaluated from the spectral plates and from Fourier transform spectra fit better to the values calculated from the pairs of energy levels of the transition.

Table 1 contains all lines for which the corresponding transitions have been excited by laser light, and for which we have observed a laser-induced fluorescence or an optogalvanic signal. The center of gravity wavelengths are determined from wavenumber calibrated Fourier transform spectra provided to us by Pickering [9] and Engleman [8] using the dispersion formula of Reeder and Peck [10] for

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 Table 1. Investigated lines of Ta I.

	Intone	4		Thom	aitian	En anora las	-1	Domonla
۱/Å	this work	[6]	[5]	dog oven	dog odd	Energy lev	ver / cm	nemark
A/A	ml 20	[0]	[0]	a <sup>4</sup> D	ues. ouu	22.226 014	46 176 770	norra lino
4175.800	ni 50 640	- 15	-	$a D_{1/2}$	$m_{3/2}$	22 230.014	40170.770	new nne a
4170.995	$m^{1}$ 70	10	10	$a D_{5/2}$	$z G_{7/2}$	12 800.907	30799.903 32.036.716	n orre line o
4 183.908	$m_{10}$	-	-	$\frac{5}{2}$	$m_{7/2}$	47 820.71	23 920.710	new line
4 184.000	<i>m</i> 55	-	-	<sup>1</sup> 7/2 <sup>2</sup> D **	<sup>III</sup> 7/2 ·	47 817.107	23 920.710	new nne
4 185.939	90 	(2)	-	$P_{3/2}$	$m_{5/2}$	15 903.818	39 786.599	
4 189.017		-	-	$a^{-}D_{3/2}$	$^{\circ}P_{3/2}^{\circ}$	21 381.052	45 240.284	new line
4 194.627	nl 660	-	-	$a^{-}P_{3/2}$	$y^{\circ}\mathrm{D}_{1/2}^{\circ}$	6 068.956	29 902.273	new line
4 196.166	nt 1	-	-	$a^{-}H_{13/2}$	$H_{11/2}^{*}$	23 514.923	47 339.489	new line
4 200.302	nl 60	-	-	$G_{9/2}^{-6}$	$m_{11/2}^{*}$	25 376.469	49177.58	new line
4 204.160	nl 100	-	-	$a^{\circ}D_{7/2}$	$S_{5/2}^{*}$	12234.772	3 6014.068	new line
4 205.258	nl 10	-	-	$G_{9/2}^{**}$	( <u>9/2</u>	25 376.469	49 149.532	new line
4 205.871	7800	300	100	$a^{-}F_{7/2}$	$z^{\circ} F_{9/2}^{\circ}$	3 963.922	27 733.511	5
4 206.381	800	120	50	$e^{\circ}F_{1/2}$	$z^{\circ}\mathrm{G}^{\circ}_{3/2}$	41 151.381	17 384.689	
4 209.175	nl 190	-	-	<sup>4</sup> F <sub>5/2</sub> ***	$m_{5/2}^{\circ}^{*}$	44 918.665	21 167.596	new line
4 212.571	nl 35	-	-	?9/2	${}^{2}\mathrm{F}_{7/2}^{\circ}^{*}$	50 692.194	26 960.484	new line
4214.261	nl 70	-	-	$?_{5/2}$	$m_{5/2}^{\circ}*$	45769.81	22047.454	new line
4219.680	nl 55	-	-	$?_{7/2}$	$z^{\mathrm{o}}\mathrm{F}^{\mathrm{o}}_{5/2}$	48872.99	25181.186	new line
4 220.129	nl 100	-	-	$?_{5/2}$	$z^2\mathrm{D}^\circ_{3/2}$	44461.647	20772.357	new line
4224.883	nl 10	-	-	$?_{13/2}$	$z^{\mathrm{o}}\mathrm{F}^{\mathrm{o}}_{11/2}$	54023.88	30361.262	new line
4226.758	nl 15	-	-	${}^{4}\mathrm{D}_{3/2}*$	$m_{5/2}^{\circ}*$	24275.959	47928.08	new line
4228.258	$nl \ 25$	-	-	$a^4\mathrm{H}_{11/2}$	${}^{2}I^{\circ}_{13/2}*$	22428.650	46072.280	new line
4229.392	nl 120	-	-	$?_{7/2}$	$m_{5/2}^{\circ}$ *	49857.127	26219.648	new line
4231.219	nl 55	-	-	$a^{2}\mathrm{F}_{5/2}$	$m_{5/2}^{\circ}^{*}$	17224.462	40851.654	new line
4231.923	$nl \ 1$	-	-	$a^4 G_{5/2}$	${}^{6}\mathrm{P}^{\circ}_{3/2}*$	21623.018	45246.284	new line
4232.502	nl 45	-	-	${}^{4}G_{7/2}$ **	$?_{5/2}^{\circ}$	24917.996	48537.973	new line
4232.923	145	35	-	${}^{4}F_{3/2}$ ***	$z^4\mathrm{D}^\circ_{3/2}$	43275.474	19657.804	
4233.699	nl 35	-	-	$?_{7/2}$	$m_{9/2}^{\circ}*$	11884.41	35497.669	new line
4235.548	nl 35	-	-	$?_{7/2}$	$z^6\mathrm{D}^\circ_{7/2}$	51383.695	27780.652	new line
4235.889	160	-	5h	$e^{6}F_{3/2}$	${}^{4}\mathrm{G}^{\circ}_{5/2}*$	41594.852	17993.726	
4236.351	nl 70	-	-	$a^2\mathrm{F}_{7/2}$	$m_{7/2}^{\circ}*$	17383.173	40981.768	new line
4236.998	nl 55	-	-	${}^{4}\mathrm{F}_{7/2}*$	$z^4\mathrm{F}^{\mathrm{o}}_{5/2}$	46958.10	23363.113	new line
4238.548	nl 35	-	-	${}^{2}\mathrm{P}_{3/2}^{**}$	${}^{6}\mathrm{F}^{\circ}_{1/2}*$	15903.818	39490.148	new line
4238.702	$nl \ 250$	-	-	$a^{6}\mathrm{D}_{3/2}$	$m_{1/2}^{\circ}$ *	9975.837	33561.282	new line
4241.071	nl 40	-	-	${}^{4}\mathrm{D}_{1/2}$ **	$?^{\circ}_{1/2}$	20144.81	43717.154	new line
4242.552	nl $65$	-	-	$?_{7/2}$	$z^6 \mathrm{G}^\circ_{9/2}$	46245.64	22681.695	new line
4246.887	$nl \ 25$	-	-	$a^4\mathrm{H}_{9/2}$	${}^{6}\mathrm{F}^{\circ}_{7/2}*$	21153.396	44693.412	new line
4249.875	$nl \ 25$	-	-	${}^{4}\mathrm{F}_{5/2}^{**}$	$?^{\circ}_{7/2}$	24546.202	48069.689	new line
4250.704	nl 70	-	-	$a^4\mathrm{H}_{7/2}$	$?^{\circ}_{7/2}$	20646.702	44165.583	new line <sup><math>c</math></sup>
4253.908	nl 40	-	-	$?_{9/2}$	${}^{6}\mathrm{D}^{\circ}_{7/2}*$	51683.81	28182.633	new line
4255.502	nl  80	-	-	$a^2 G_{7/2}$	$z^6\mathrm{P}^\circ_{7/2}$	9705.350	33197.724	new line
4256.897	$nl \ 100$	-	-	$?_{5/2}$	$z^4\mathrm{D}^{\mathrm{o}}_{3/2}$	43142.50	19657.804	new line
4257.807	nl 110	-	-	$a^2 G_{7/2}$	$\mathrm{m}_{5/2}^{\circ}{}^{*}$	9705.350	33185.006	new line
4259.833	nl 15	-	-	$a^2 \mathrm{F}_{7/2}$	$m_{5/2}^{\circ}*$	17383.173	40851.654	new line
4263.048	nl 40	-	-	$a^2 P_{1/2}$	${}^{4}\mathrm{P}^{\circ}_{3/2}*$	11792.152	35242.955	new line
4263.494	105	(1)	-	$a^6\mathrm{D}_{9/2}$	$z^4 \mathrm{G}^\circ_{7/2}$	13351.546	36799.905	d
4268.232	nl 450	-	-	$e^{6}\mathrm{F}_{7/2}$	$z^6 \mathrm{G}^\circ_{7/2}$	43982.532	20560.317	new line
4270.264	nl 15	-	-	${}^{4}\mathrm{H}_{7/2}**$	${}^{6}\mathrm{D}^{\circ}_{7/2}*$	22761.279	46172.492	new line
4274.266	nl 15	-	-	$?_{5/2}$	${}^{4}\mathrm{G}^{\circ}_{7/2}*$	45769.81	22380.481	new line
4276.805	nl 15	-	-	${}^{4}G_{5/2}$ **	$m_{3/2}^{\circ}*$	23512.447	46887.789	new line

	Interaid			There is a second secon		En anora las	$ral / am^{-1}$	Domonia
) / Å	Intensi	[c]	[=1	1rans	sition	Energy lev	vel / cm	Remark
λ/Α	this work	[6]	[5]	des. even	des. odd	even	000	1:
4 290.753	nl 20	-	-	$P_{1/2}$	°D <sub>3/2</sub> "	49889.45	26 590.053	new line
4 291.735	ni 40	-	-	(5/2 2D	$m_{5/2}^{-1}$	44 461.647	21 167.596	new line
4 291.867	nl 55	-	-	$a^{-}D_{5/2}$	$z$ $\mathrm{H}_{7/2}$	12865.967	36 159.292	new line,
4 000 000	1.00			40 *	400	40.000 57	04.001.000	blend
4 292.906	nl 80	-	-	G <sub>9/2</sub> <sup>+</sup>	$z^{-}F_{7/2}$	48 269.57	24 981.880	new line
4 294.386	1030	55	-	$a^{\circ}D_{9/2}$	$m_{9/2}^{*}$	13 351.546	36 631.213	1.
4 297.485	nt 150	-	-	$a^{\circ}D_{7/2}$	$m_{9/2}^{*}$	12 234.772	35 497.669	new line
4 297.893	$nl \ 90$	-	-	${}^{4}G_{9/2}^{*}$	$z$ °G $_{11/2}$	48 269.57	25 008.899	new line
4 298.882	nl 15	-	-	$D_{7/2}^{**}$	( <u>9</u> /2 2D0	25 894.092	49 149.532	new line
4310.597	$nl \ 40$	-	-	?3/2	$z^2 D_{3/2}^{\circ}$	43 964.474	20772.357	new line
4312.431	$nl \ 200$	-	-	$?_{11/2}$	$z^{\circ}\mathrm{F}^{\circ}_{9/2}$	50915.638	27733.511	new line <sup>e</sup>
4317.377	nl 40	-	-	${}^{2}P_{3/2}$ **	$m_{5/2}^{\circ}*$	15903.818	39059.531	new line
4317.535	$nl \ 1$	-	-	$a4G_{11/2}$	$m_{11/2}^{\circ}^{*}$	26022.739	49177.58	new line
4319.274	$nl \ 270$	-	-	$a^{4}{ m F}_{9/2}$	$z^{\circ}\mathrm{D}_{9/2}^{\circ}$	5621.123	28766.644	new line
4320.864	nl 35	-	-	$a^4\mathrm{D}_{3/2}$	${}^{4}\mathrm{P}^{\circ}_{1/2}*$	21381.052	44518.050	new line
4322.681	360	65	5	$a^2\mathrm{F}_{7/2}$	$z^4 \mathrm{G}^{\circ}_{11/2}$	17383.173	40510.392	
4325.001	$nl \ 100$	-	-	$a^2 F_{5/2}$	$m^{\circ}_{3/2}*$	17224.462	40339.329	new line
4325.702	$nl \ 100$	-	-	$a^4 \mathrm{H}_{11/2}$	$m_{9/2}^{\circ}$ *	22428.650	45539.801	new line
4326.183	nl 15	-	-	$a^2 \mathrm{F}_{5/2}$	$m^{\circ}_{7/2}*$	17224.462	40333.027	new line
4329.644	nl 110	-	-	$e^6\mathrm{F}_{3/2}$	$z^4\mathrm{D}^{\mathrm{o}}_{1/2}$	41594.852	18504.755	$new line^{f}$
4330.857	$nl \ 25$	-	-	${}^{4}\mathrm{G}_{9/2}*$	${}^{4}\mathrm{G}^{\circ}_{9/2}*$	48269.585	25185.964	new line
4331.541	nl 10	-	-	$a^{2}\mathrm{H}_{11/2}$	$z^{4}\mathrm{H}^{\circ}_{11/2}$	15114.280	38194.285	new line
4334.647	nl 45	-	-	${}^{4}\mathrm{F}_{5/2}$ ***	$z^4 \mathrm{F}^{\circ}_{3/2}$	4918.665	21855.124	new line
4336.998	$nl \ 250$	-	-	${}^{6}\mathrm{D}_{3/2}$ **	$m_{5/2}^{\circ}*$	10950.262	34001.203	new line
4340.681	nl 150	-	-	${}^{4}\mathrm{F}_{7/2}*$	$m_{7/2}^{\circ}*$	46958.10	23926.716	new line
4344.301	370	85	20	$a^{4}\mathrm{H}_{9/2}$	$?^{\circ}_{7/2}$	21153.396	44165.583	
4344.606	nl  80	-	-	$a^{2}D_{5/2}$	$m_{5/2}^{\circ}*$	12865.967	35876.551	new line
4348.869	nl $65$	-	-	$a^{4}\mathrm{H}_{9/2}$	$m_{11/2}^{\circ}*$	21153.396	44141.422	new line
4351.950	nl 110	-	-	$a^4\mathrm{F}_{5/2}$	$z^{4} F_{7/2}^{\circ}$	2010.134	24981.880	new line
4352.427	nl 55	-	-	$a^{4}D_{3/2}$	$m_{3/2}^{\circ}*$	21381.052	44350.284	new line
4353.893	nl 150	-	-	$a^{4}P_{5/2}$	$m_{3/2}^{\circ}*$	9253.453	32214.941	new line
4355.090	280	110	80	$e^{6}F_{9/2}$	$z^6 G^{\circ}_{0/2}$	45636.874	22681.695	
4357.697	nl 75	-	-	${}^{2}\mathrm{P}_{3/2}^{**}$	$m_{1/2}^{\circ}*$	15903.818	38845.286	new line
4360.175	nl 90	-	-	?3/2	$m_{5/2}^{\circ}*$	44096.008	21167.596	$new line^{g}$
4363.833	nl 30	-	-	?9/2	${}^{6}F^{\circ}_{11/2}*$	50692.194	27783.084	new line
4369.033	nl 25	-	_	${}^{4}G_{7/2}$ **	${}^{2}\mathrm{H}^{\circ}_{0/2}*$	24917.996	47 799,909	new line
4371.100	nl 90	-	_	${}^{4}F_{5/2}^{***}$	$m_{r}^{\circ}$	44 918.665	22047.454	new line <sup>h</sup>
4 398.771	nl 60	-	_	$a^{4}G_{5/2}$	$m_{2/2}^{0/2}$	21 623.018	44 350.284	new line
4 401.764	nl 1	-	_	$a^2 \mathbf{F}_{\mathbf{F}/2}$	${}^{4}D^{\circ}_{7/2}$	17224.462	39,936,246	new line
4 404.389	nl 1	-	_	${}^{4}D_{2/2}*$	$^{4}S^{\circ}_{2}$	24275.959	46 974.209	new line
4 407 745	nl 15	_	_	?= /2	$m_{-2}^{2}$	53 271 95	30 590 985	new line
4 413 121	$nl \ 10$	_	_	· 5/2 ?_/2	$m_{7/2}^{\circ}$	48 872 99	26 219 648	new line
4 420 203	nl 40	-	_	?7/2	$z^{6}D^{\circ}_{2}$	51383695	28766644	new line
4 427 025	nl 45	_	_	· //2 ?= /2	$z^{6}G^{\circ}_{-}$	43 142 50	20,560,317	new line <sup>i</sup>
4 485 800	150	- (1)	-	$^{\cdot 5/2}$	$\sim 07/2$	11709150	34 078 456	IICW IIIIC
4 513 588	nl 35	(1)	-	2 1 1/2 ?	$^{113/2}_{2^{6}D^{\circ}}$	50.015.638	28 766 644	new line <sup>b</sup>
5670 543	nl = 0	-	-	$^{\cdot 11/2}$	$^{\sim} D_{9/2}^{-4} D^{\circ} *$	25 876 05	43 478 915	new line
5773 170	$n_{1}$ 1	-	-	$^{4}D_{4} **$	$m^{\circ}$ *	20 01 0.00	37/61/85	new line
0110.119	100 1	-	-	$\nu_{1/2}$	<b>111</b> 1/2	20144.01	01 101.400	new mile

 Table 1. Continued.

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	Intensi	ty		Trans	sition	Energy le	Remark	
$\lambda/{ m \AA}$	this work	[6]	[5]	des. even	des. odd	even	odd	
6047.185	$nl \ 1$	-	-	${}^{2}\mathrm{H}_{9/2}**$	$\mathrm{m}_{7/2}^{\circ}{}^*$	29116.264	45648.307	new line
6547.870	$nl \ 15$	-	-	$a^2 D_{5/2}$	$y^4\mathrm{D}^\circ_{5/2}$	12865.967	28133.941	new line
6611.909	800	110	300	$a^6 D_{5/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}*$	11243.656	26363.721	
6653.666	$nl \ 1$	-	-	${}^{2}\mathrm{H}_{9/2}**$	$m_{11/2}^{\circ}$ *	29116.264	44141.422	new line
6776.640	10	-	2	$?_{3/2}$	$\mathrm{m}^{\circ}_{5/2}*$	44096.008	29343.501	
6787.542	1	(1)	-	$e^6 F_{3/2}$	${}^{6}\mathrm{D}^{\circ}_{1/2}*$	41594.852	26866.045	

Table 1. Continued.

If not marked otherwise, designations are taken from reference [13], \* designations are taken from reference [14], m mixed configuration, largest eigenvalue component below 25%, \*\* designation as given in reference [1], \*\*\* designation as given in [15], <sup>a</sup> also observed as fluorescence line when exciting the transition belonging to the line  $\lambda = 4263.53$  Å, <sup>b</sup> this transition appeared also as a negative fluorescence line when exciting  $\lambda = 4312.44$  Å and as a positive fluorescence line when exciting  $\lambda = 6450.36$  Å, <sup>c</sup> also observed as fluorescence line when exciting the line  $\lambda = 4344.301$  Å, <sup>d</sup> also observed as fluorescence line when exciting the line  $\lambda = 4344.301$  Å, <sup>d</sup> also observed as fluorescence line when exciting the line  $\lambda = 4344.301$  Å, <sup>d</sup> also observed as fluorescence line when exciting the line  $\lambda = 4346.301$  Å, <sup>f</sup> also observed as fluorescence line when exciting the line  $\lambda = 6786.59$  Å, <sup>g</sup> also observed as fluorescence line when exciting the line  $\lambda = 4209.175$  Å, <sup>i</sup> also observed as fluorescence line when exciting the line  $\lambda = 4209.175$  Å, <sup>i</sup> also observed as fluorescence line when exciting the line  $\lambda = 4209.175$  Å, <sup>i</sup> also observed as fluorescence line when exciting the line  $\lambda = 4209.175$  Å, <sup>i</sup> also observed as fluorescence line when exciting the line  $\lambda = 4209.175$  Å, <sup>i</sup> also observed as fluorescence line when exciting the line  $\lambda = 4256.89$  Å.

The list contains lines which are already classified if new lines could be found or up to now unassignable lines could be classified when exciting them.

the refraction index of air; the accuracy is better than  $\pm 0.005$  Å. When a line mentioned is not visible in the Fourier spectra, we give the wavelength calculated from the energy levels, again using the refraction index of air [10].

When the lines in Table 1 were already classified earlier, the excitation did lead to the discovery of at least one ore some new fluorescence lines. For such lines the intensities as given in references [5–7] are listed. For all investigated lines, we give the intensity taken from Fourier transform spectra of Engleman [8]. These intensities are uncorrected concerning instrument and detector sensitivity; the light source for these spectra was a Ta hollow cathode lamp driven with  $\sim 300$  mA. The noise level is dependent on wavelength and is approximately 5 at 4 300 Å and 1 at 7 000 and 3 000 Å. If a weak line could not be found in the Fourier spectrum but only at the photo plate, we gave it the intensity 1.

When the transitions listed in Table 1 are excited, the upper levels decay to a large manifold of other lower levels and emit thereby fluorescence light which shows the same intensity modulation like the chopped exciting laser light. If the monochromator is tuned to such a fluorescence line, a LIF signal is detected by our lock-in amplifier. When then the laser is tuned over a certain range (up to 0.2 Å), the LIF signal shows the typical hyperfine pattern of the excited transition. Most of the observed fluorescence lines could be assigned to already classified transitions and are therefore not mentioned. Another manifold of fluorescence lines could be classified for the first time. These lines are listed in Table 2. For the wavelengths and intensities of Table 2 the same is valid as for Table 1. For lines, which could not be found in the Fourier spectra, but for which a LIF signal was observed, the calculated wavelength and the intensity 1 is given. In some cases the new classified

fluorescence lines coincide with fluorescence lines of nearly the same wavelengths which belong to other transitions. Such blend situations are mentioned in Table 2. Fluorescence lines which are not listed in references [5–7] are indicated as nl (new line). In column 9 of Table 2 the exciting laser wavelengths are listed.

In some cases the investigated new spectral lines could not be assigned to a pair of known levels. That means that at least one up to now unknown level takes part in the transition. A good fit of the recorded hyperfine pattern using programs developed in Hamburg [11,12] gave us the opportunity to determine the J-values and the hyperfine constants A and B of the levels involved. Using a pair of A and B values as a "fingerprint" for a fine structure level, in most cases one of the levels of the involved transition could be identified. The other level could then be calculated using the wavenumber of the line. In other cases the unknown (upper) level could be determined by comparing the wavenumber difference between excitation wavelength and a fluorescence line with wavenumber differences between known levels.

14 previously unknown levels were discovered in such way within the present work. Some of them could be excited on several transitions, confirming in this way their existence. The properties of the new discovered levels are listed in Table 3. Some of these levels were already included in a parametric fine and hyperfine structure analysis and their configuration and designation could be calculated [14]. Taking into account results given in reference [2] and two of the levels mentioned in Table 3, all states of the  $e^4F$  of the configuration  $5d^36s7s$  are now identified. We will try to identify the levels designated as  $e^4F$  in reference [13] in forthcoming papers.

As an example, we discuss a special part of the investigations now in more detail. Figure 1 shows the hyperfine

Table 2	able 2. Lines classified via laser-induced fluorescence.										
	Trans	sition	Energy le	$evel/cm^{-1}$	Excitation	Remark					
[5]	des. even	des. odd	even	odd	$\lambda/{ m \AA}$						
-	$a^4 F_{7/2}$	$?^{\circ}_{5/2}$	3963.92	48537.973	4232.502	classified					
-	$a^4 F_{3/2}$	$m^{\circ}_{3/2}*$	0	44350.284	4398.771						
-	$a^4 F_{3/2}$	$?_{1/2}^{\circ}$	0	43717.154	4241.071						
5	$a^4 F_{9/2}$	$m_{11/2}^{\circ}*$	5621.04	49177.58	4200.302	classified					
-	$a^4 F_{3/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}*$	0	43478.215	5679.543						
-	$a^4 P_{3/2}$	$?^{\circ}_{5/2}$	6068.956	48537.973	4232.502						
-	$a^4 P_{3/2}$	$m^{\circ}_{3/2}*$	6068.956	46176.77	4175.806						
70	$a^6\mathrm{D}_{3/2}$	$?^{\circ}_{5/2}$	9975.837	48537.973	4232.502	classified					
-	$a^{4}F_{9/2}$	$?^{\circ}_{7/2}$	5621.04	44165.58	4344.301	$\mathbf{blend}^{\mathbf{a}}$					
15	$a^4 P_{1/2}$	?°.	604942	13717 154	4 241 071						

Т

	Intensi	ty		Trans	sition	Energy le	$\mathrm{vel}/\mathrm{cm}^{-1}$	Excitation	Remark
$\lambda/{ m \AA}$	this work	[6]	[5]	des. even	des. odd	even	odd	$\lambda/{ m \AA}$	
2242.762	-	4	-	$a^4 F_{7/2}$	$?^{\circ}_{5/2}$	3963.92	48537.973	4232.502	classified
2254.083	$nl \ 1$	-	-	$a^{4}F_{3/2}$	$m_{3/2}^{\circ}*$	0	44350.284	4398.771	
2286.73	$nl \ 25$	-	-	$a^{4}F_{3/2}$	$?_{1/2}^{\circ}$	0	43717.154	4241.071	
2295.166	15	160	5	$a^{4}F_{9/2}$	$m_{11/2}^{\circ}$ *	5621.04	49177.58	4200.302	classified
2299.295	$nl \ 1$	-	-	$a^{4}F_{3/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}*$	0	43478.215	5679.543	
2353.938	$nl \ 1$	-	-	$a^{4}P_{3/2}$	?°/2	6068.956	48537.973	4232.502	
2492.530	nl 12	-	-	$a^{4}P_{3/2}$	$m_{3/2}^{\circ}*$	6068.956	46176.77	4175.806	
2592.437	13	12 h	70	$a^{6}\mathrm{D}_{3/2}$	$?_{5/2}^{\circ}$	9975.837	48537.973	4232.502	classified
2593.633	nl 30	-	-	$a^{4}F_{9/2}$	$?^{\circ}_{7/2}$	5621.04	44165.58	4344.301	$blend^{a}$
2654.009	25	21	15	$a^{4}P_{1/2}$	$?^{\circ}_{1/2}$	6049.42	43717.154	4241.071	
2672.338	25	-	20	$a^{4}P_{3/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}$ *	6068.956	43478.215	5679.543	
2753.764	$nl \ 1$	-	-	$a^{6}\mathrm{D}_{7/2}$	$?_{5/2}^{\circ}$	12234.772	48537.973	4232.502	
2790.443	$nl \ 1$	-	-	$a^{6}\mathrm{D}_{9/2}$	$m_{11/2}^{\circ}*$	13351.546	49177.58	4200.302	
2848.428	$nl \ 1$	-	-	$a^{4}P_{5/2}$	$m_{3/2}^{\circ}*$	9253.453	44350.284	4398.771	
2907.426	nl 1	-	-	$a^2 P_{1/2}$	$m_{3/2}^{\circ}*$	11792.152	46176.770	4175.806	
2934.852	28	70	40	$a^{2}\mathrm{H}_{11/2}$	$m_{11/2}^{\circ}*$	15114.280	49177.58	4200.302	classified
2940.090	nl $65$	-	-	$a^{6}\mathrm{D}_{5/2}$	${}^{6}\mathrm{P}^{\circ}_{3/2}$ *	11243.656	45246.284	4189.017	
2964.811	15	-	3w	$a^{6} D_{1/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}$ *	9759.017	43478.215	5679.543	
2983.991	nl 1	-	-	$a^{6}D_{3/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}$ *	9975.837	43478.215	5679.543	
2988.695	$nl \ 25$	-	-	$a^{6}\mathrm{D}_{5/2}$	${}^{6}\mathrm{F}^{\circ}_{7/2}*$	11243.656	44693.412	4246.887	
3050.978	nl 10	-	-	${}^{6}\mathrm{D}_{3/2}^{**}$	?° :1/2	10950.262	43717.154	4241.071	
3131.440	$nl \ 20$	-	-	$a^{2}P_{1/2}$	?° ?1/2	11792.152	43717.154	4241.071	
3155.043	$nl \ 20$	-	-	$a^{2}P_{1/2}$	${}^{4}\mathrm{D}^{\circ}_{1/2}$ *	11792.152	43478.215	5679.543	
3175.276	nl 1	-	-	$a^{2}D_{5/2}$	$m_{3/2}^{\circ}*$	12865.967	44350.284	4398.771	
3237.483	nl 12	-	-	?7/2	${}^{4}\text{G}^{\circ}_{5/2}*$	48872.99	17993.726	4219.680	
3243.355	50	28	-	?7/2	$z^6 G^{\circ}_{7/2}$	51383.695	20560.317	4 4 20. 203,	classified
				1/2	1/2			4 235.548	
3258.658	nl 12	-	-	$?_{7/2}$	$z^6 \mathrm{G}^\circ_{5/2}$	49857.127	19178.426	4229.392	
3306.840	nl 12	-	-	${}^{4}P_{1/2}^{*}$	$z^{4} D^{\circ}_{2/2}$	49889.45	19657.804	4290.753	
3308.543	15	-	20	?7/2	$m_{5/2}^{\circ}*$	51383.695	21167.596	4235.548	classified
3351.705	nl 1	-	-	?5/2	${}^{4}\text{G}^{\circ}_{5/2}*$	47820.71	17993.726	4183.968	
3366.654	120	45	50	?7/2	$z^{6}G_{5/2}^{\circ}$	48872.99	19178.426	4219.680	classified
3412.368	$nl \ 20$	-	-	?7/2	$z^{6} G^{\circ}_{7/2}$	49857.127	20560.317	4229.392	
3445.508	70	-	2h	$?_{13/2}$	$z^{6} G^{\circ}_{11/2}$	54023.88	25008.899	4224.859	
3558.872	nl 1	-	-	?5/2	$z^{6} F^{\circ}_{5/2}$	53271.95	25181.186	4407.745	
3566.037	1	-	7	${}^{4}P_{1/2}^{*}$	$z^{4} F^{\circ}_{3/2}$	49889.45	21855.124	4290.753	
3567.326	95	-	4	$a^{4}H_{9/2}$	$m_{11/2}^{\circ}*$	21153.33	49177.58	4200.302	classified
3594.383	nl 15	-	-	${}^{2}P_{3/2}^{**}$	?° •1/2	15903.818	43717.154	4241.071	
3628.493	nl 30	-	-	$a^{6}D_{7/2}$	$m_{5/2}^{\circ}*$	12234.772	39786.599	4185.939	
3638.427	$nl \ 8$	-	-	?7/2	${}^{4}\text{G}^{\circ}_{7/2}*$	49857.127	22380.481	4229.392	
3658.395	nl 17	-	-	$a^{4}P_{5/2}$	$y^{4}F_{3/2}^{\circ}$	9253.453	36580.06	4215.714	
3667.757	nl 45	-	-	?7/2	$z^6 G_{7/2}^\circ$	47817.167	20560.317	4184.600	
3678.747	nl 1	-	-	?7/2	$z^6 G^{\circ}_{0/2}$	49857.127	22681.695	4229.392	
3696.031	nl 1	-	-	?5/2	$z^2 D_{3/2}^{\circ}$	47820.71	20722.357	4183.968	
3710.742	nl 15	-	-	$a^{2}F_{5/2}$	$?^{\circ}_{7/2}$	17224.462	44165.583	4344.301	blend <sup>b</sup>
3714.346	$nl \ 20$	-	-	$a^{4}G_{5/2}$	?%	21 623.018	48 537.973	4 232.502	
3737.430	nl 10	-	-	$a^{4}\mathrm{H}_{11/2}$	$m_{11/2}^{\circ}$ *	22428.650	49177.58	4 200.302	
3743.981	nl 100	_	-	?9/2	$z^{4} F_{7/2}^{\circ}$	51 683.79	24981.880	4 253.908	
3759.559	nl 75	_	-	?5/2	$z^6 G^{\circ}_{r/2}$	45769.81	19178.426	4214.271	
				. 0/ 4	5/2				

Table 2. Continued.

	Intensit	v		Trans	sition	Energy le	$vel/cm^{-1}$	Excitation	Remark
$\lambda/{ m \AA}$	this work	, [6]	[5]	des. even	des. odd	even	odd	$\lambda/\text{Å}$	Homain
2765 020	ml 19			°4D	° *	01 201 OF9	47.029.09	4 226 752	
3703.832 3773375	nl 15 nl 35	-	-	$u D_{3/2}$	$r^{4}\mathrm{F}^{\circ}_{-}$	49857127	47 928.08 23 363 113	4 220.758	
3 777 086	nl 380	_	-	·7/2 ?= /2	$^{2}$ $^{1}$ $^{5/2}$ $^{4}$ $^{\circ}$ $^{*}$	44 461 647	17003726	4 220.002	
3 800 470	nl 380 $nl$ 1	-	-	$\frac{15/2}{a^4 C}$	$m^{\circ}$ *	21 623 018	17 993.120	4 220.129	
2 800.470	ml = 70	-	-	$u G_{5/2}$	${}^{6}C^{\circ}$ *	54 022 88	47 920.00 27 778 002	4 220.100	
3 809.023	$\frac{11}{10}$	-	-	$^{+13/2}$	G <sub>13/2</sub>	0 705 29	21 110.095	4 224.000	
3 8 19.909		-	-	$u G_{7/2}$	$\frac{111_{5/2}}{40^{\circ}}$ *	9705.50	17002796	4 220.000	
3 8 2 9 . 9 9 9	m 00	-	-	· 3/2	$G_{5/2}$	44 090.008	17 995.720 21 855 124	4 300.173	
3 0 3 0 . 1 0 0		-	-	$\frac{15}{2}$	$z \Gamma_{3/2}$	47 020.71 50 015 745	21 000 000	4 103.900	
3 0 3 0 . 0 0 9 2 9 9 5 4 4 0	m l = 40	-	-	$\frac{11/2}{2}$	$2 G_{11/2}$	50 915.745	25 000.099 DE 18E 064	4 312.431	
3 000.449	m 40	-	-	:11/2	$G_{9/2}$	30 913.743	23 185.904	4 512.451,	
2 200 672	95	0		41. **	<b>9</b> 0	00 0 40 05 1	49 597 079	4 010.000	-1:6-1
3890.078	20	2	-	F <sub>3/2</sub>	<sup>1</sup> 5/2	22 842.851	48 337.973	4 232.302	classified
3 895.009	nl 1	-	-	$a_{13/2}$	$m_{11/2}$	23 314.923	49177.38	4 200.302	
3 898.138		-	-	$P_{1/2}$	$z^{*}F_{3/2}$	49 889.45	24 243.447	4 290.753	
3 906.481	ni (	-	-	(3/2 2	$z^{-}D_{1/2}^{-}$	44 096.008	18 504.755	6776.640	1 . 6 1
3 919.488	100	40	-	(9/2 2	$G_{9/2}^{*}$	50 692.194	25 185.964	4212.571	classified
3 929.665	nl 15	-	-	(5/2 411 **	$G_{7/2}^{*}$	47 820.71	22 380.481	4 183.968	
3 956.976	nl 30	-	-	$^{+}\text{H}_{9/2}^{**}$	$m_{11/2}^{*}$	23 912.929	49177.58	4 200.302	
3957.591	nl 25	-	-	*F <sub>5/2</sub> ***	$z^{\star}\mathrm{D}^{\circ}_{3/2}$	44 918.665	19657.804	4 209.175	
3965.648	nl 20	-	-	?5/2	$z^{\circ}\mathrm{G}^{\circ}_{7/2}$	45 769.81	20 560.317	4274.266	
3 972.386	nl 15	-	-	<sup>4</sup> H <sub>7/2</sub> **	$m_{5/2}^{\circ}$	22761.279	47 928.08	4225.76	
3975.211	nl 17	-	-	? <sub>5/2</sub>	${}^{4}G_{5/2}^{\circ}*$	43 142.50	17993.726	4 256.897	
3985.284	nl 13	-	-	<sup>4</sup> F <sub>3/2</sub> **	$m_{5/2}^{\circ}*$	22842.851	47 928.08	4 226.758	
3986.661	nl 1	-	-	$e^{\circ}F_{9/2}$	$z^{\mathrm{o}}\mathrm{G}^{\mathrm{o}}_{7/2}$	45 636.874	20560.317	4355.090	
3994.791	nl 1	-	-	${}^{4}G_{5/2}^{**}$	$?_{5/2}^{\circ}$	23512.447	48537.973	4 232.502	
4000.570	nl 30	-	-	$?_{11/2}$	$m_{9/2}^{\circ}*$	50915.745	25926.383	4312.431,	
					4			4513.588	
4018.936	nl 30	-	-	$?_{7/2}$	$z^4\mathrm{F}^{\mathrm{o}}_{7/2}$	49857.127	24981.880	4229.392	
4035.881	$nl \ 250$	-	-	${}^{4}F_{3/2}$ ***	$z^4\mathrm{D}^{\mathrm{o}}_{1/2}$	43275.474	18504.755	4232.923	blend <sup>c</sup>
4051.397	nl 90	-	-	$?_{7/2}$	$z^{\circ}\mathrm{F}^{\circ}_{5/2}$	49857.127	25181.186	4229.392	
4052.171	$nl \ 1$	-	-	$?_{7/2}$	${}^{4}\mathrm{G}^{\circ}_{9/2}*$	49857.127	25185.964	4229.392	
4069.663	nl 75	-	-	$a^{\mathrm{o}}\mathrm{D}_{7/2}$	$z^4\mathrm{G}^\circ_{7/2}$	12234.772	36799.905	4176.993	
4088.145	$nl \ 10$	-	-	?7/2	$z^4\mathrm{F}^{\mathrm{o}}_{5/2}$	47817.167	23363.113	4 184.600	
4094.581	nl 5	-	-	${}^{4}G_{5/2}$ **	$m_{5/2}^{\circ}*$	23512.447	47928.08	4226.758	
4118.064	90	19	5	${}^{4}\mathrm{F}_{7/2}^{*}$	$z^{\mathrm{o}}\mathrm{G}^{\mathrm{o}}_{9/2}$	46958.10	22681.695	4340.681	classified
4120.491	nl 45	-	-	${}^{4}\mathrm{D}_{3/2}*$	$?_{5/2}^{\circ}$	24275.959	48537.973	4232.502	
4129.329	nl 350	-	-	$e^{\circ}\mathrm{F}_{3/2}$	$z^{\mathfrak{b}}\mathrm{G}^{\mathfrak{o}}_{3/2}$	41594.852	17384.689	6787.542,	
								4329.644	
4148.709	$nl \ 25$	-	-	${}^{4}\mathrm{F}_{3/2}$ ***	$z^6 \mathrm{G}^\circ_{5/2}$	43275.474	19178.426	4232.923	
4171.736	nl  80	-	-	$?_{5/2}$	$z^6 \mathrm{G}^\circ_{5/2}$	43142.50	19178.426	4256.897	
4200.302	nl 60	-	-	${}^{4}G_{9/2}$ **	$m^{\circ}_{11/2}$	25376.469	49177.58	4317.535	new line
4250.704	nl 70	-	-	$a^4\mathrm{H}_{7/2}$	$?^{\circ}_{7/2}$	20646.702	44165.583	4344.301	е
4275.613	$nl \ 1$	-	-	${}^{4}\mathrm{F}_{5/2}$ **	$m_{5/2}^{\circ}*$	24546.202	47928.08	4226.758	
4329.644	nl 110	-	-	$e^{6}\mathbf{F}_{3/2}$	$z^4\mathrm{D}^\circ_{1/2}$	41594.852	18504.755	6787.542,	f
								4235.889	
4331.228	nl 1	-	-	$?_{5/2}$	$z^6\mathrm{D}^\circ_{3/2}$	47820.71	24739.060	4183.968	
4334.647	nl 45	-	-	${}^{4}\mathrm{F}_{5/2}$ ***	$z^4 \mathrm{F}^{\circ}_{3/2}$	44918.665	21855.124	4209.175	g
4334.867	$nl \ 20$	-	-	$?_{7/2}$	$z^6\mathrm{D}^\circ_{5/2}$	49857.127	26794.812	4229.392	

 Table 2. Continued.

	Intensit	y		Trans	sition	Energy le	$\mathrm{vel}/\mathrm{cm}^{-1}$	Excitation	Remark
$\lambda/{ m \AA}$	this work	[6]	[5]	des. even	des. odd	even	odd	$\lambda/{ m \AA}$	
4360.175	nl 90	-	-	?3/2	$m_{5/2}^{\circ}*$	44 096.008	21167.596	6776.640	h
4371.100	nl 90	-	-	${}^{4}\mathrm{F}_{5/2}^{***}$	$m_{5/2}^{\circ}*$	44918.665	22047.454	4209.175	i
4414.427	$nl \ 25$	-	-	$e^{6}F_{1/2}$	$z^{4} D_{1/2}^{\circ}$	41 151.381	18504.755	4 206.381	
4427.025	nl 45	-	-	?5/2	$z^{6}G^{\circ}_{7/2}$	43142.50	20560.317	4256.897	
4434.815	nl  10	-	-	$a^{4}G_{5/2}$	?~/2	21623.018	44165.583	4344.301	
4435.639	$nl \ 25$	-	-	${}^{4}\mathrm{F}_{5/2}$ ***	${}^{4}G^{\circ}_{7/2}*$	44918.665	22380.481	4209.175	
4474.375	nl  140	-	-	${}^{4}G_{9/2}^{*}$	$m_{0/2}^{\circ}*$	48269.585	25926.383	4 292.906	
4475.819	nl 50	-	-	$a^4 D_{3/2}$	9/2 ?0	21381.052	43717.154	4241.071	
4479.216	$nl \ 100$	-	-	?7/2	$m_{7/2}^{\circ}*$	46245.64	23926.716	4242.552	
4513.588	nl 35	-	-	?11/2	$z^6 \dot{\mathrm{D}}^{\circ}_{0/2}$	50915.745	28766.644	4312.431	j
4522.003	$nl \ 25$	-	-	${}^{4}F_{3/2}***$	$m_{5/2}^{\circ}*$	43275.474	21167.596	4232.923	
4557.221	nl 1	-	-	$e^{6}F_{3/2}$	$z^{4} D^{\circ}_{2/2}$	41594.852	19657.804	4235.889	$blend^k$
4591.740	nl  145	-	-	${}^{4}\mathrm{F}_{7/2}^{*}$	${}^{4}G^{\circ}_{0/2}*$	46958.10	25185.964	4236.998	
4628.100	nl 75	-	-	?5/2	$m_{5/2}^{\circ}*$	47820.71	26219.648	4 183.968	
4637.897	nl 50	-	-	${}^{4}F_{5/2}$ ***	$z^4 F_{E/2}^{\circ}$	44918.665	23363.113	4209.175	
4651.253	nl 20	-	-	$e^{6}F_{1/2}$	$z^{4} D^{\circ}_{2/2}$	41 151.381	19657.804	4 206.381	
4669.650	nl 120	-	-	$a^{2}H_{9/2}$	$z^{4}G^{\circ}_{7/2}$	15391.019	36 799.905	4176.993	
4670.649	nl 1	-	-	${}^{4}\mathrm{H}_{7/2}^{**}$	?~/2	22761.279	44165.583	4344.301	
4703.581	nl 1	-	-	$e^{6}F_{3/2}$	$z^{2}S_{1/2}^{\circ}$	41594.852	20340.405	4235.889	
4708.853	nl 1	_	_	?5/2	${}^{6}D_{2/2}^{\circ}*$	47 820.71	26590.053	4 183.968	
4755.510	nl 35	-	-	?7/2	$z^6 D_{r/2}^\circ$	47 817.167	26794.812	4 184.600	
4789.258	155	_	4	${}^{4}F_{2/2}**$	$2^{\circ}_{11}$	22 842 851	43717.154	4 241.071	classified
4 793.287	nl 40	_	-	- 3/2 ?7/2	${}^{2}F_{\pi/2}^{\circ}*$	47 817.167	26 960.484	4 184.600	crassifica
4 803.814	nl 1	_	_	$e^{6}F_{1/2}$	$z^{2}S_{1}^{\circ}$	41 151.381	20340.405	4 206.381	
4815.143	nl 120	_	_	?= 1/2	${}^{4}G^{\circ}_{7/2}*$	43 142.50	22 380.481	4 256.897	blend <sup>1</sup>
4 835.386	nl 90	_	_	${}^{4}F_{5/2}$	$z^6 F_{2/6}^\circ$	44 918.665	24243.447	4 209.175	
4 840.091	nl 25	_	_	$e^{6}$ Fo/2	$z^4 F_{\pi/2}^{\circ}$	45 636.874	24 981.880	4 355.090	
4 840.522	nl 20	_	_	${}^{4}G_{5/2}^{**}$	$2^{\circ}_{7/2}$	23 512.447	44 165.583	4 344.301	
4 905.636	nl = 0 nl = 60	_	_	$e^{6}F_{1/2}$	$\frac{r^{7/2}}{z^2 D_{o}^{\circ}}$	41 151.381	20772.32	4 206.381	
4 936 247	$nl \ 1$	_	_	${}^{4}\text{H}_{0/0}**$	≈ ± 3/2 ?°_ (2	23 912 929	44 165 583	4 344 301	
4 958 110	nl 120	_	_	${}^{4}F_{7/2}^{*}$	$z^{6}D^{\circ}_{z}$	4695810	26 794 812	4 340 681	blend <sup>m</sup>
4 988 625	nl 35	_	_	?= //2	$z^6 D_{-10}^2$	4782071	27780.652	4 183 968	biolita
5035731	nl 50	_	_	· 5/2 ?2/2	$z^6 F^{\circ}_{2}$	44 096 008	24243447	6 776 640	
5054357	nl 80	_	_	· 3/2 ?= /9	$z^4 F^{\circ}_{z}$	4314250	23363113	4 256 897	
5 095 581	nl = 1	_	_	•5/2 <sup>4</sup> Fr./0**	~ 1 5/2 ?° (2	24546202	44165583	4 344 301	
5 114 349	nl 15	_	_	$e^{6}F_{2/2}$	$\frac{1}{2}$ m <sup>o</sup> <sub>2</sub> (*	41 594 852	22.047.454	4 235 889	
5119.037	nl 25	_	_	2 ± 3/2 ?7/2	$m_{5/2}^{\circ}$	48 872 99	29 343 501	4 219 680	
5194 006	50	20	_	$^{4}G_{7}$ (2)	?°_/2	24 917 996	44 165 583	4 344 301	blend <sup>n</sup>
5 208 648	nl 1	-	_	~1/2 ?⊧/2	$\frac{\cdot 7/2}{m_{0}^{\circ}/2}$	53 271 95	34078456	4 407 745	Siona
5 213 058	nl 1	_	_	· 5/2 ?= /2	$u^6 D^\circ_{-}$	53 271 95	34 094 692	4 407 745	
5 223 236	nl 45	_	_	$a^4 H_{\pi/2}$	$y = \frac{1}{7/2}$ m <sup>o</sup> <sub>c</sub> *	20 646 702	39786 599	4 185 939	
5310845	nl 45	_	_	${}^{4}F_{\pi/0}*$	$\frac{115}{2}$	46 958 10	28 133 941	4 340 681	blend <sup>o</sup>
5 320 750	nl 10	_	_	$^{4}G_{0/2}^{**}$	9 - 5/2	25376469	44 165 583	4 344 301	SIGILA
5 324 613	nl 25	_	_	$^{4}F_{7/2}$	·7/2 <sup>6</sup> D⁰*	46 958 10	28 182 633	4 236 998	
5 352 862	nl 20	_	_	$e^{6}F_{0,10}$	$^{2}F^{\circ}_{-}$ *	45 636 874	26 960 484	4 355 090	
5 454 465	nl 25	_	_	<sup>4</sup> F <sub>2</sub> /- ***	<sup>+</sup> 7/2 <sup>6</sup> D°*	44 918 665	26 500.464	4 200 175	
5478490	nl = 30	_	_	$^{15/2}$	<sup>6</sup> D° *	48 260 585	20 090.000	4 330 857	
0410.400	111 50	-	-	$G_{9/2}$	$D_{9/2}$	40 203.000	50 021.272	4 202 006	
								4 292.900, 1 207 202	
								4 291.090	

Intensity			Transition		Energy le	Energy level $/  \mathrm{cm}^{-1}$		Remark	
$\lambda/{ m \AA}$	this work	[6]	[5]	des. even	des. odd	even	odd	$\lambda/{ m \AA}$	
5516.090	nl 30	-	-	${}^{4}\mathrm{F}_{5/2}$ ***	$z^6\mathrm{D}^\circ_{5/2}$	44918.665	26 794.812	4209.175	
5524.023	nl 30	-	-	$?_{5/2}$	$m_{7/2}^{\circ}*$	47820.71	29722.985	4183.968	
5534.590	$nl \ 13$	-	-	$?_{7/2}$	${}^{6}\mathrm{D}^{\circ}_{7/2}*$	46245.64	28182.633	4242.552	
5545.333	nl 110	-	-	$a^2 G_{7/2}$	$z^{6} F^{\circ}_{9/2}$	9705.38	27733.511	4205.871	$\mathbf{blend}^{\mathbf{p}}$
5565.970	$nl \ 15$	-	-	$?_{5/2}$	$z^6 \mathrm{F}^{\circ}_{5/2}$	43142.50	25181.186	4256.897	
5566.976	nl $22$	-	-	${}^{4}\mathrm{F}_{5/2}**$	${}^{2}\mathrm{F}^{\circ}_{7/2}$ *	44918.665	26960.484	4334.647	
5637.862	$nl \ 12$	-	-	$?_{3/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}*$	44096.008	26363.721	6776.640	
5881.434	$nl \ 1$	-	-	${}^{4}G_{5/2}**$	$z^4 \mathrm{G}^{\circ}_{11/2}$	23512.447	40510.392	4322.681	
5958.254	nl 5	-	-	$?_{5/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}$ *	43142.50	26363.721	4256.897	
5997.641	$nl \ 1$	-	-	${}^{4}\mathrm{G}_{9/2}*$	$m_{7/2}^{\circ'}*$	48269.585	31600.982	4292.906	
6038.241	$nl \ 10$	-	-	$?_{5/2}$	$z^{6} F^{\circ}_{7/2}$	43142.50	26585.979	4256.897	
6039.730	$nl \ 1$	-	-	$?_{5/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}*$	43142.50	26590.053	4256.897	q
6098.619	$nl \ 1$	-	-	$?_{5/2}$	$m_{5/2}^{\circ}*$	47820.71	31428.092	4183.968	
6100.380	$nl \ 1$	-	-	$a^{6}D_{3/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}*$	9975.837	26363.721	6611.909	
6392.618	$nl \ 1$	-	-	$e^{6}F_{1/2}$	$y^4\mathrm{D}^\circ_{1/2}$	41151.381	25512.63	4206.381	
6479.908	nl 17	-	-	${}^{4}\mathrm{F}_{7/2}*$	${}^{4}\mathrm{H}^{\circ}_{9/2}$ *	46958.10	31530.050	4340.681	$\mathbf{blend}^{\mathbf{r}}$
6502.182	$nl \ 1$	-	-	$e^{6} F_{3/2}$	$m_{5/2}^{\circ}*$	41594.852	26219.648	4235.889	
6577.464	nl 22	-	-	${}^{4}\mathrm{G}_{9/2}*$	${}^{4}\mathrm{H}^{\circ}_{11/2}$ *	48269.57	33070.364	4292.906	
6662.692	nl 5	-	-	$e^{6}F_{3/2}$	${}^{6}\mathrm{D}^{\circ}_{3/2}$ *	41594.852	26590.053	4235.889	
6767.498	$nl \ 1$	-	-	${}^{4}\mathrm{G}_{9/2}*$	$m_{9/2}^{\circ}*$	48269.585	33497.154	4292.906	
8026.010	nl 95	-	-	${}^{4}G_{9/2}^{*}$	${}^{4}G_{11/2}^{*}$	48269.585	35813.517	4292.906	

Table 2. Continued.

If not marked otherwise, designations are taken from reference [13], \* designation as given in reference [14], m mixed configuration, largest eigenvalue component below 25%, \*\* designation as given in reference [1], \*\*\* designation as given in reference [15], <sup>a</sup> blend situation with 2593.660 Å, ionic line 42 959.55 - 4415.79 cm<sup>-1</sup> [16], <sup>b</sup> blend situation with 3710.777 Å, 42 844.673 - 15 903.818 cm<sup>-1</sup> [17], <sup>c</sup> blend situation with 4 035.893 Å, 35 720.898 - 10 950.22 cm<sup>-1</sup>, <sup>e</sup>, <sup>f</sup>, <sup>g</sup>, <sup>h</sup>, <sup>i</sup>, <sup>j</sup> these transitions were also excited, <sup>k</sup> blend situation with 4 557.241 Å, 43 090.337 - 21 153.396 cm<sup>-1</sup>, <sup>1</sup> blend situation with 4 815.137 Å, 46 981.974 - 26 219.648 cm<sup>-1</sup>, <sup>m</sup> blend situation with 4 958.110 Å, 46 958.10 - 26 794.812 cm<sup>-1</sup>, <sup>n</sup> blend situation with 5 193.886 Å, 36 631.213 - 17 383.173 cm<sup>-1</sup>, <sup>o</sup> blend situation with 5 310.965 Å, 41 585.022 - 22 761.279 cm<sup>-1</sup>, <sup>p</sup> blend situation with 5 545.153 Å, 30 894.719 - 12 865.967 cm<sup>-1</sup>, <sup>q</sup> or 6 038.241 was excited or both, <sup>r</sup> blend situation with 6 479.930 Å, 46 981.974 - 31 553.879 cm<sup>-1</sup>, <sup>s</sup> blend situation with 7 043.457 Å, 32 187.394 - 17 993.726 cm<sup>-1</sup>. Already known lines are marked as classified.

structure of the new line  $\lambda = 4\,200.302$  Å. The line is not listed in the wavelength tables, but we could determine a wavelength of  $4\,200.32$  Å from the photo plate.

Because we are able to set the wavelength of our exciting laser with an accuracy of 0.01 Å, we positioned the laser wavelength in steps of 0.01 Å around this value. At each step we scanned the monochromator until we observed laser-induced fluorescence. With the monochromator fixed at the fluorescence wavelength we scanned the laser around 4 200.32 Å and recorded the hyperfine pattern of the corresponding transition (for obtaining hyperfine constants). Then we set the laser to the strongest hyperfine component and looked for further fluorescence lines. We found 3 fluorescence lines originating from the upper level: 2 295.166 Å, an unclassified line with the relative intensity 5 [5], a new line at 2 790.443 Å, and a further unclassified line at 2 934.852 Å, with the relative inten-

sity 70 [6]. Each of those lines showed the same hyperfine pattern when scanning the laser frequency.

By combining the wavenumbers of the excited transition and the fluorescence lines we found that the excited transition must have 25 376.469 cm<sup>-1</sup>, 9/2 even as its lower level. By adding the wave number of the exciting laser light we could now calculate the energy of a new upper level to be 49 177.58  $\pm$  0.03 cm<sup>-1</sup>. The lower levels of the three fluorescence lines had even parity and J = 9/2 or 11/2, so the new one must have odd parity and J = 11/2 or 9/2. Finally a value of J = 11/2 followed from the analysis of the hyperfine pattern. Later on four further fluorescence lines could be observed which were calculated as possible decays from the new level: 3567.326 Å, an unclassified transition with the relative intensity 4 [5], and the new lines 3737.430 Å, 3895.609 Å and 3956.976 Å. In order to determine the hyperfine constants A and B

Configuration	Designation	Energy $/\mathrm{cm}^{-1}$	$A\ /\ {\rm MHz}$	$B\ /\ {\rm MHz}$	$\lambda_{ m exc}/{ m \AA}$
even parity					
	$?_{5/2}$	43142.50	254(5)	1840(100)	4256.897,4171.736,4427.025
	$?_{5/2}$	45769.74	577(8)	260(30)	4274.266,4214.271
	?7/2	46245.79	282.9(52)	298(30)	4242.552
$5d^{3}6s7s$	${}^{4}\mathrm{F}_{7/2}^{***}$	46958.11	725(4)	-520(60)	4236.998,4340.681
	?5/2	47820.71	1107(4)	-966(100)	4 183.968
$5d^{3}6s7s$	${}^{4}\mathrm{F}_{9/2}^{***}$	48269.585	982.5(20)	-1065(20)	4292.906,4297.893,4330.857
	?7/2	48872.99	-572(1)	-743(50)	4413.121, 4219.680
$5d^{3}6s7s$	${}^{4}P_{1/2}^{*}$	49889.45	3375(5)	0	4 290.753
	$?_{11/2}$	50915.745	813.6(30)	-261(80)	4312.431, 4513.588
	?7/2	51383.695	823(5)	377(90)	4420.203,4235.548
	?9/2	51683.81	630(5)	-230(50)	4253.908
	$?_{5/2}$	53271.95	1058(2)	-790(20)	4 407.745
	$?_{13/2}$	54023.88	1078(20)	-1640(100)	4 224.859
odd parity					
$5d^36s7p$	$m_{11/2}^{\circ}*$	49177.58	493(10)	3020(100)	4200.302,4317.571

Table 3. New energy levels.

If not marked otherwise, designations are taken from reference [13], \* Configuration and designation as given in reference [14] (for 49 889.45 cm<sup>-1</sup> the configuration  $5d^36s7s$  is given, since we assume that  $5d^5$  does not much contribute to the value of A, as is shown in ref. [1]), m mixed configuration, largest eigenvalue component below 25%, \*\*\* Configuration and designation as given in reference [15].



Fig. 1. Hyperfine structure of the Ta I-line  $\lambda = 4\,200.302$  Å (transition between the levels 25 376.469 cm<sup>-1</sup>, J = 9/2, even and the new level 49 177.58 cm<sup>-1</sup>, J = 11/2, odd). (a) Level scheme, (b) simulation of the hfs-spectrum using the evaluated A- and B-factors, (c) recorded hyperfine pattern and best fit result. Lower trace: difference between fitted curve and measurement (divided by a factor 3).

of the new level, we used the iterative least squares fitting procedure mentioned before [11,12] and adjusted a calculated spectrum to the measured one. For this procedure we used the already known hyperfine constants of the lower level and considered the theoretical intensity ratio of the hyperfine components. Much later on, when the Fourier spectra were available, we really found the line with a center of gravity wavelength 4 200.302 Å. The new level was included in a fine structure calculation [14], it turned out that no dominant wave function is present, we therefore call it a mixed (m) level. So the new line finally can be classified as

$$m_{11/2}^{\circ}(49\,177.58\ cm^{-1}) - {}^{4}G_{9/2}(25\,376.469\ cm^{-1}).$$

The new level could be confirmed by exciting the line 4317.535 Å, belonging to the transition:

$$m_{11/2}^{\circ}(49\,177.58\,\mathrm{cm}^{-1}) - a^4 \mathrm{G}_{11/2}(26\,022.739\,\mathrm{cm}^{-1}).$$

From the fit of the recorded hyperfine patterns of both lines, 4 200.302 Å and 4 317.535 Å we obtained mean values of the hyperfine constants: A = 493(10) MHz and B = 3020(100) MHz.

## 4 Conclusion

Although many lines have been successfully investigated in recent years, we could clearly classify a large number of additional lines obtained from our spectral plates. In some cases we discovered unknown energy levels, enlarging the knowledge of the fine structure of the Ta I atom using the hyperfine structure of the spectral lines. Further investigations are in progress. We would like to thank B. Arcimowicz (Poznan Techn. Univ.) for allowing us to use his spectral plates and J. Pickering (Imperial College London) and R. Engleman (Univ. of New Mexico, Albuquerque) for providing us with Ta Fourier transform spectra. From R. Engleman we also have got revised energy values for most of the Ta levels. Further thanks are devoted to G. Guthöhrlein and D. Messnarz (Univ. der Bundeswehr, Hamburg) for stimulating discussions. The work was supported by Jubiläumsfonds der Österreichischen Nationalbank, project no. 7079.

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